



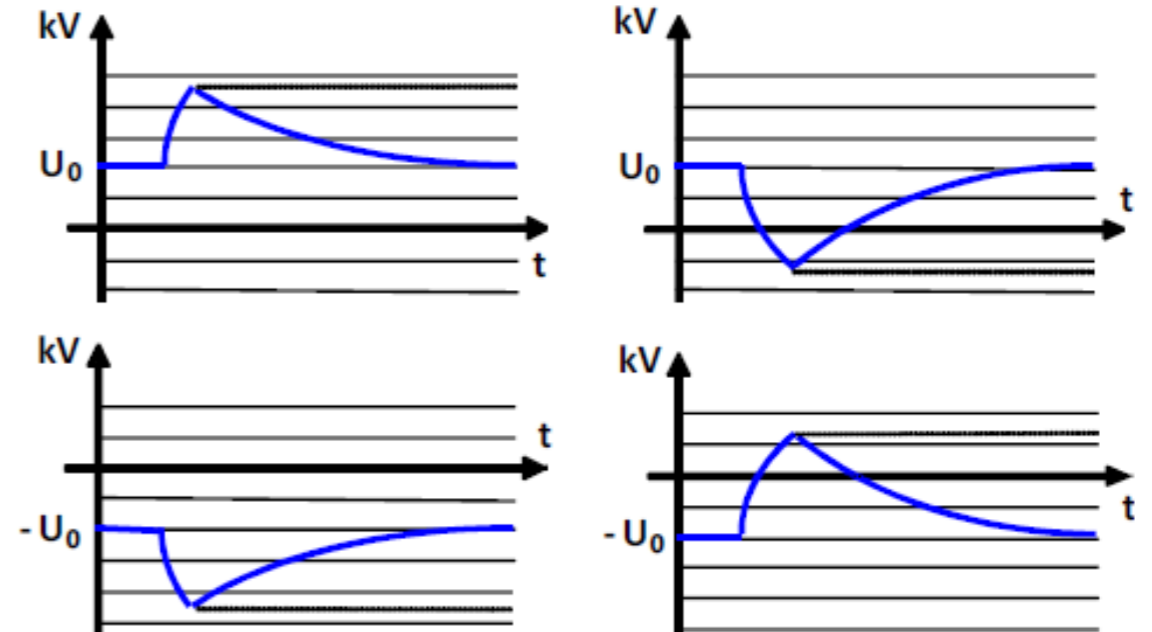
# HV-COM<sup>2</sup> - WORKING PACKAGE 3 EXISTING MEASURING SYSTEMS AT TESTING LABORATORIES

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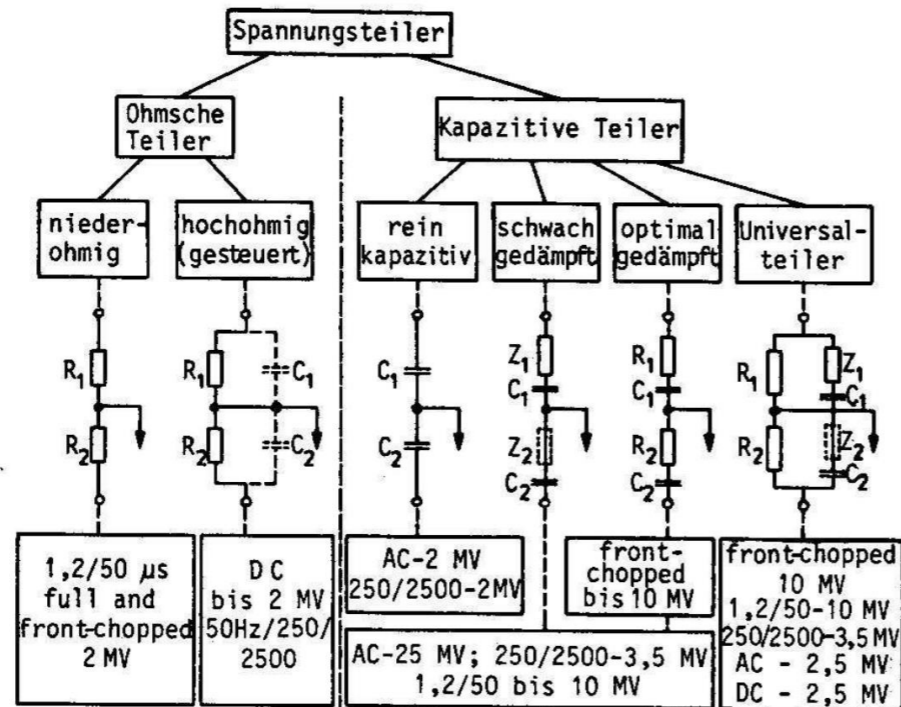
# Motivation

- Power equipment in operation is stressed by operating voltage and superimposed impulse voltages
- Realistic replication in laboratory  $\Rightarrow$  superimposed voltage tests
- Most common: DC + lightning impulse (LI) or switching impulse (SI)
  - Dielectric testing of gas-insulated HVDC systems (CIGRE TB 842)
  - Testing of extruded HVDC cables (CIGRE TB 852, IEC 62895)

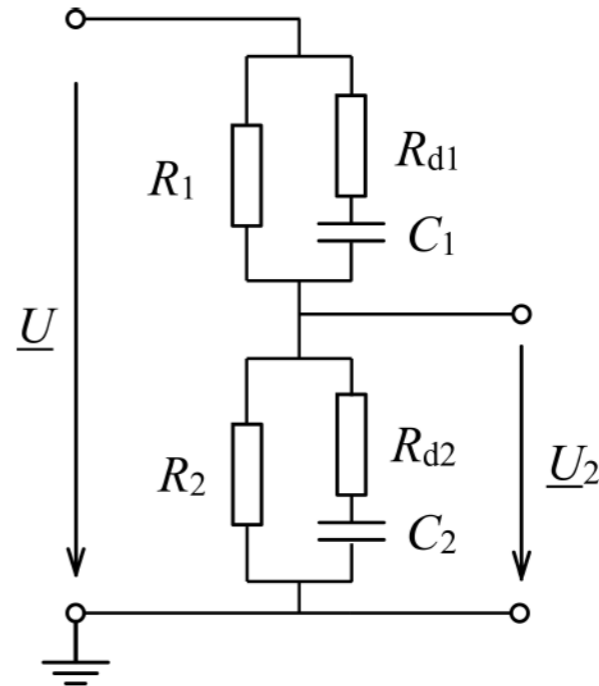


# Motivation

- It is mandatory to measure the generated superimposed test voltage directly at the test object
- Measurement is ideally performed with a resistive-capacitive divider (RC divider)
  - Widest frequency range: damped RC divider  $\Rightarrow$  universal voltage divider (RCR)  $\Rightarrow$  AC, DC, SI, LI



Ref: Modrusan



## Motivation

- **Universal voltage dividers are not yet subject to any form of standardization**
- **Calibration and linearity verification are unclear**
- Example of normative gap: IEC 62895 for the testing of HVDC cables
  - Tests with superimposed voltages required  $\Rightarrow$  ... *in accordance with IEC 60060-2* ...
  - ... *measurement of **individual** voltage components according to IEC 60060-2* ...
  - Possibility of mutual influence due to the superposition is neglected
  - Change of divider's capacitance due to DC bias?  $\Rightarrow$  influence on impulse voltage measurement

## Research questions at HV-com<sup>2</sup> – WP3

- For tests with superimposed voltages: Does the presence of one voltage waveform influence the performance of a measurement system based on universal voltage dividers with respect to the other voltage waveform?
- Point of view of calibration: Is it sufficient to calibrate measurement systems for composite voltages with the respective voltage forms individually, or is it necessary to perform it with composite voltages?
- Practical point of view: Does a DC voltage affect the measurement of superimposed LI/SI?



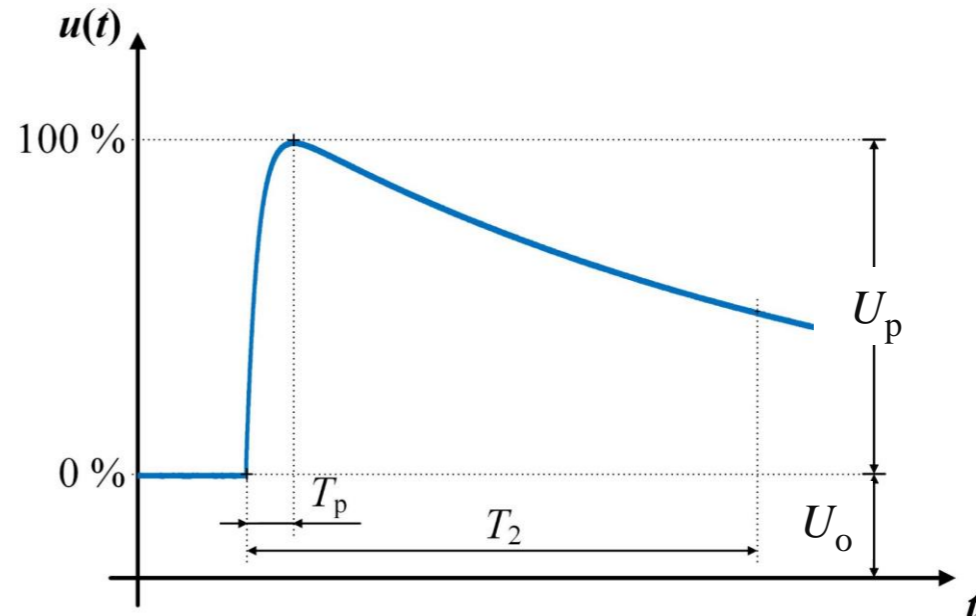
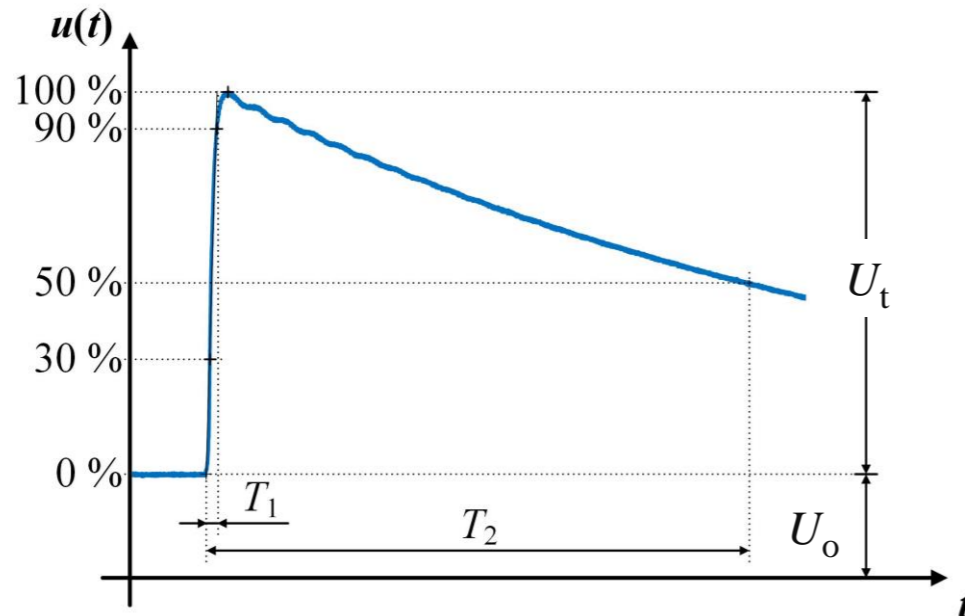
The EMPIR initiative is co-funded by the European Union's Horizon 2020 research and innovation programme and the EMPIR Participating States

- Focus on composite DC + LI/SI (two terminal test objects)



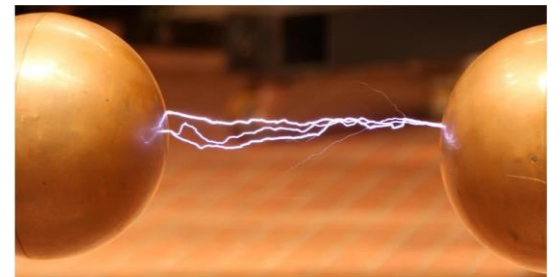
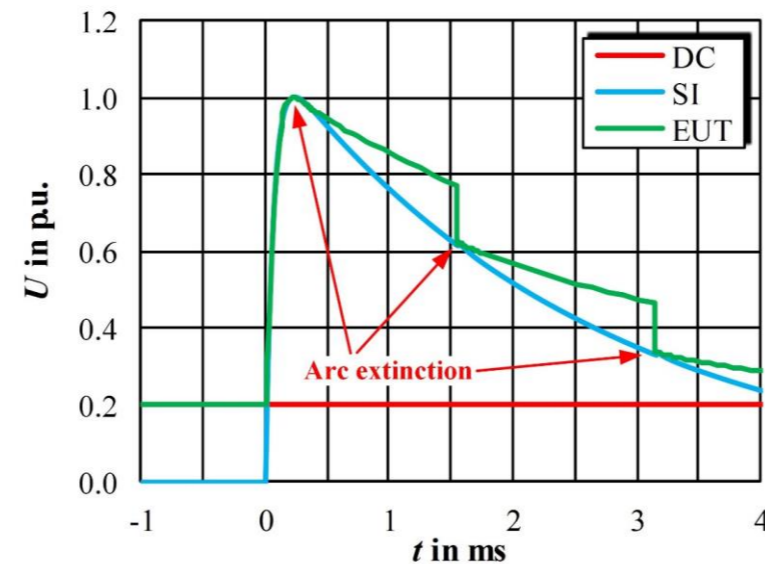
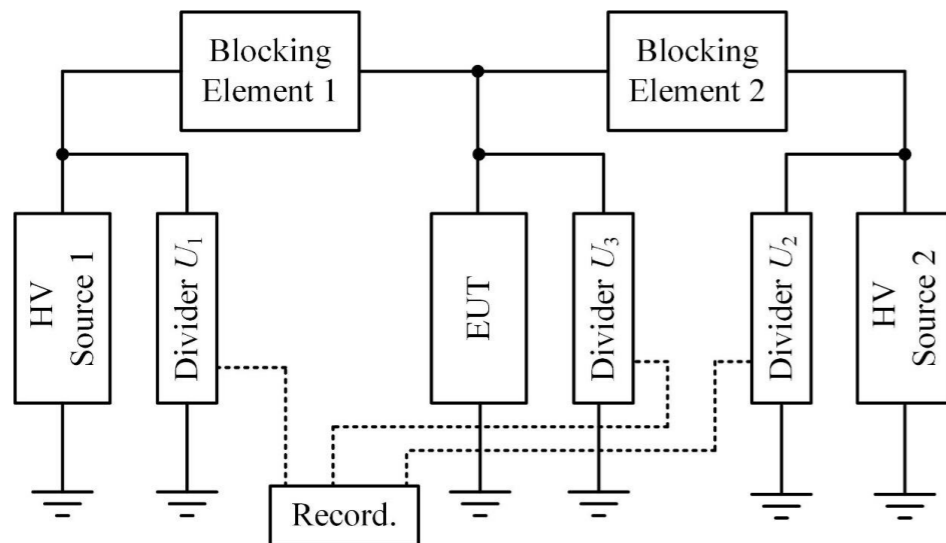
# Approach

- Comparison of commercially available RCR dividers with reference divider in **comparison campaign**
- Reference universal voltage divider was developed and tested in HV-com<sup>2</sup> project
- Evaluation of measurement error (deviation) regarding voltage and time parameters

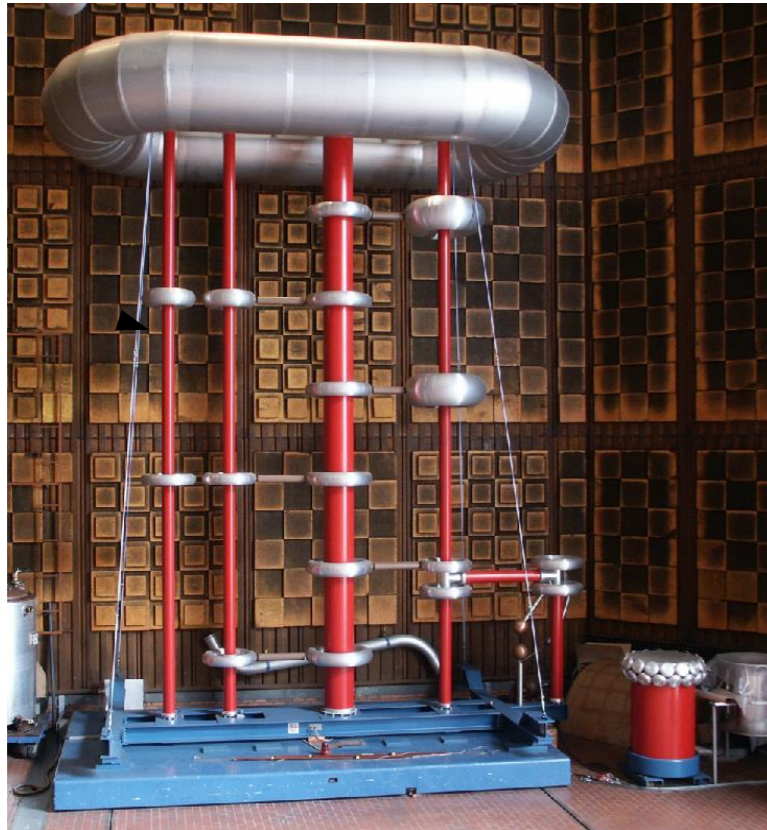


## Definition of test circuit

- Superimposed test voltages are created by combining a DC source and an impulse generator (LI/SI)
  - Blocking and coupling elements are needed to protect the sources from mutual influence
    - DC source protected with resistor
    - Impulse generator: blocking spark gap or blocking capacitor possible
- ⇒ TUG supports the use of **blocking capacitor**

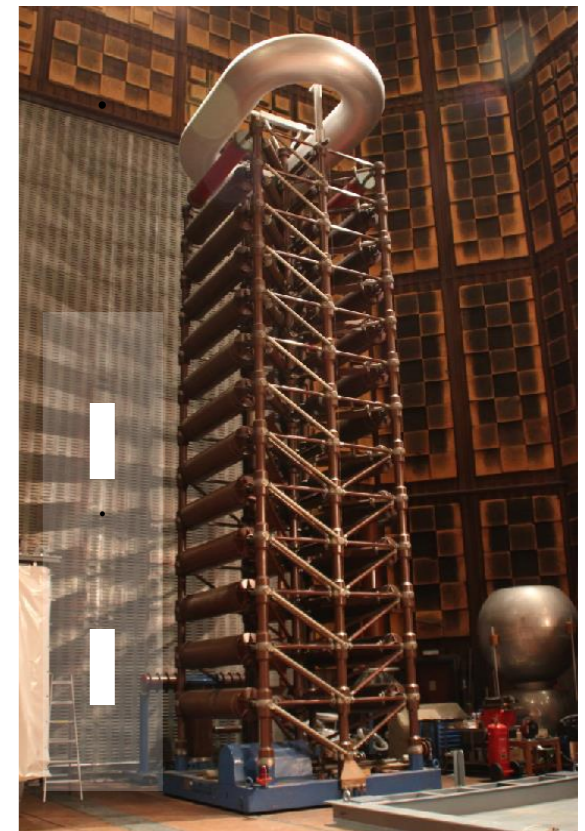
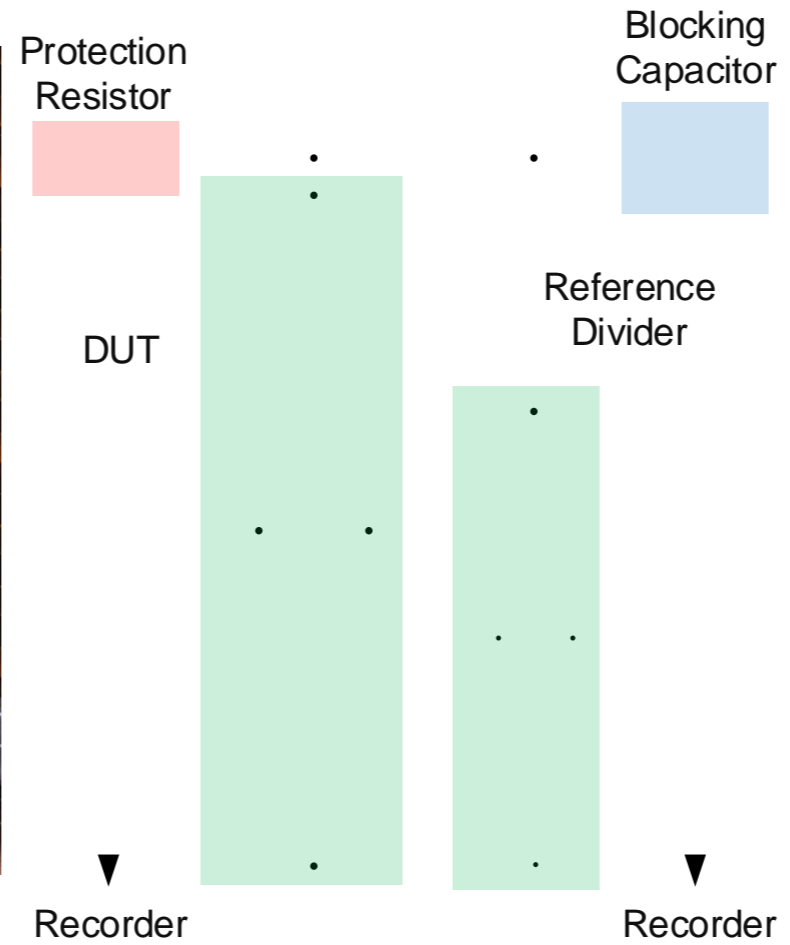


# Test circuit



$U_{DC}$   
DC: 1500 kV, 20 mA

R Divider



$U_{LI/SI}$  Impulse: 3250 kV, 165 kJ

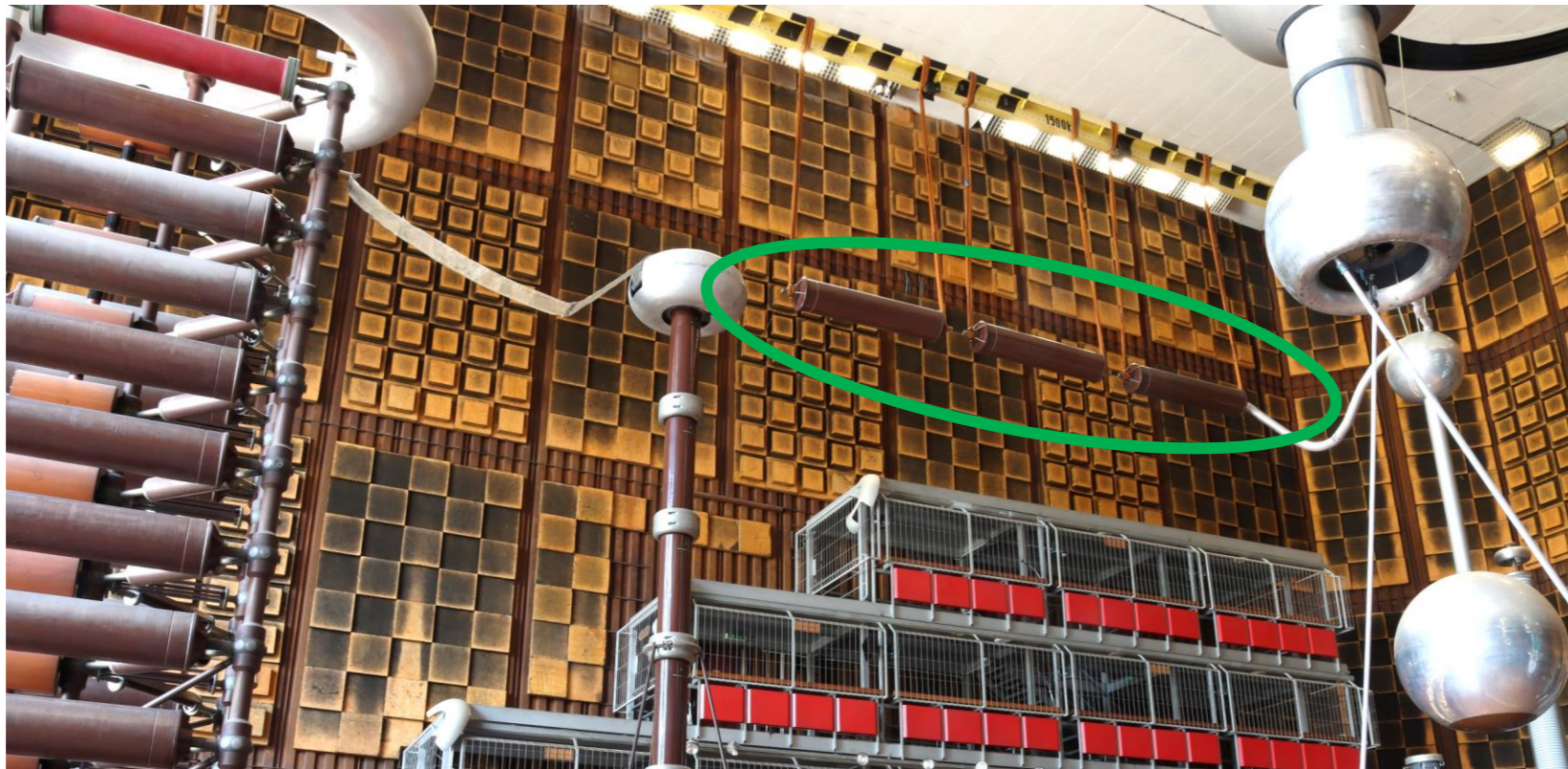
Damped Capacitive Divider

HV Laboratory: 35 m × 25 m × 21 m



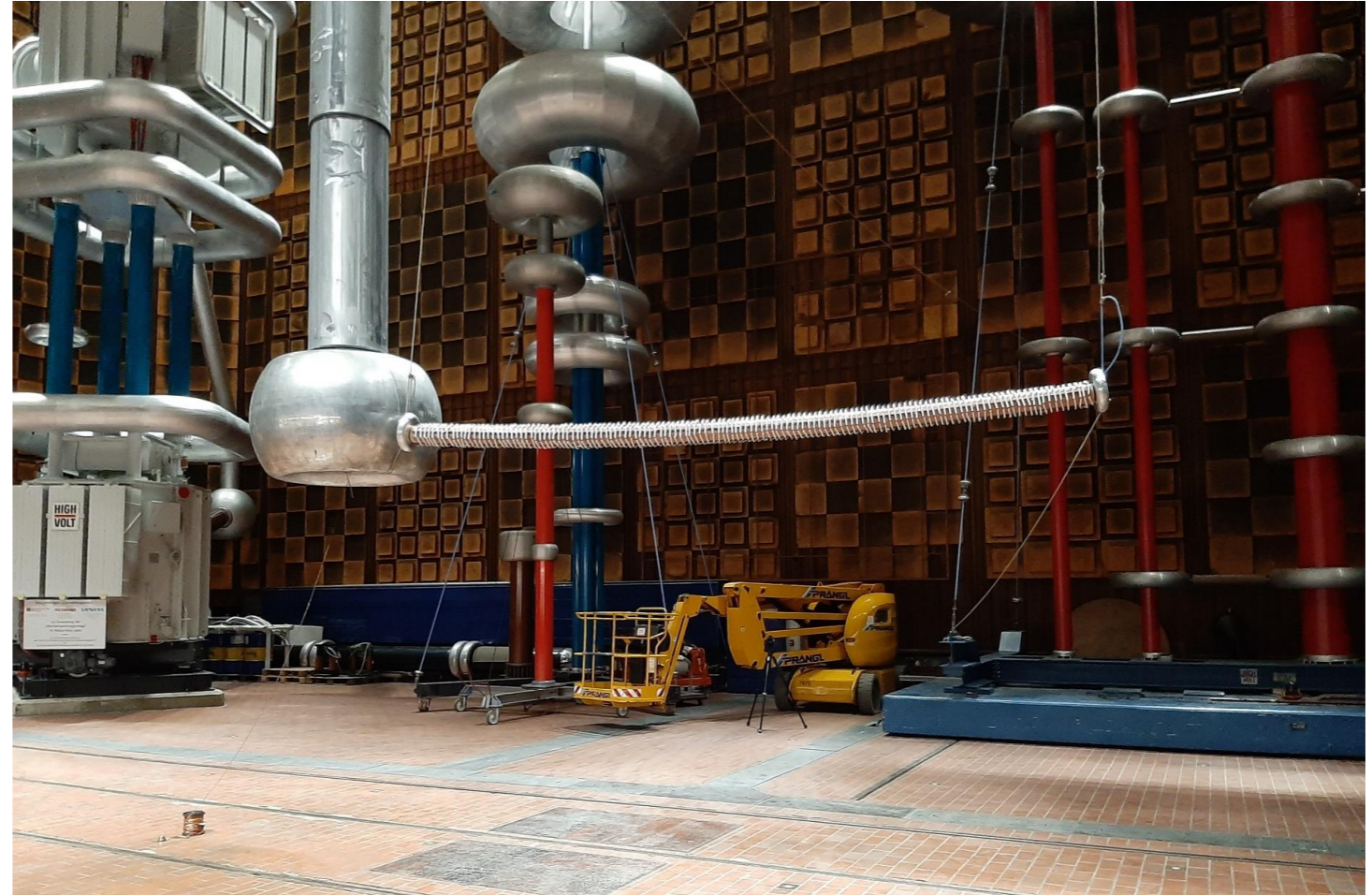
# Blocking and coupling elements

- Coupling capacitor
  - 3 capacitors in series (each 200 nF, 2.6 m, 250 kV)



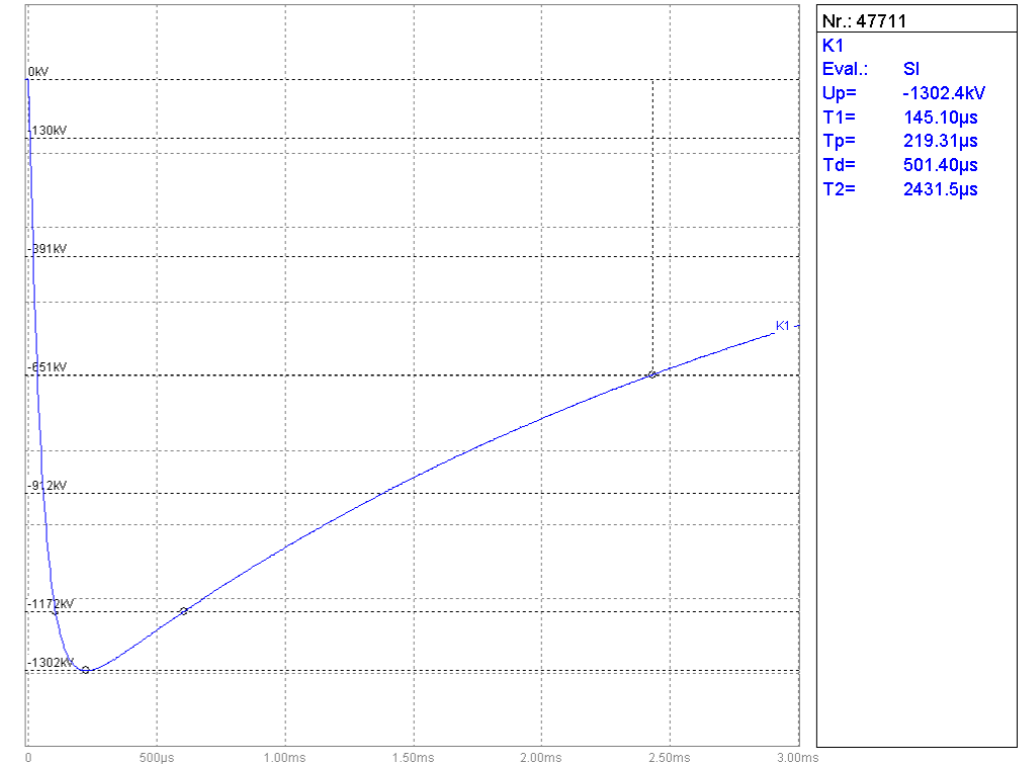
# Blocking and coupling elements

- Protection resistor
  - Taylor made by TUG
  - $R = 23 \text{ M}\Omega$   
(approx. 750 individual resistors)

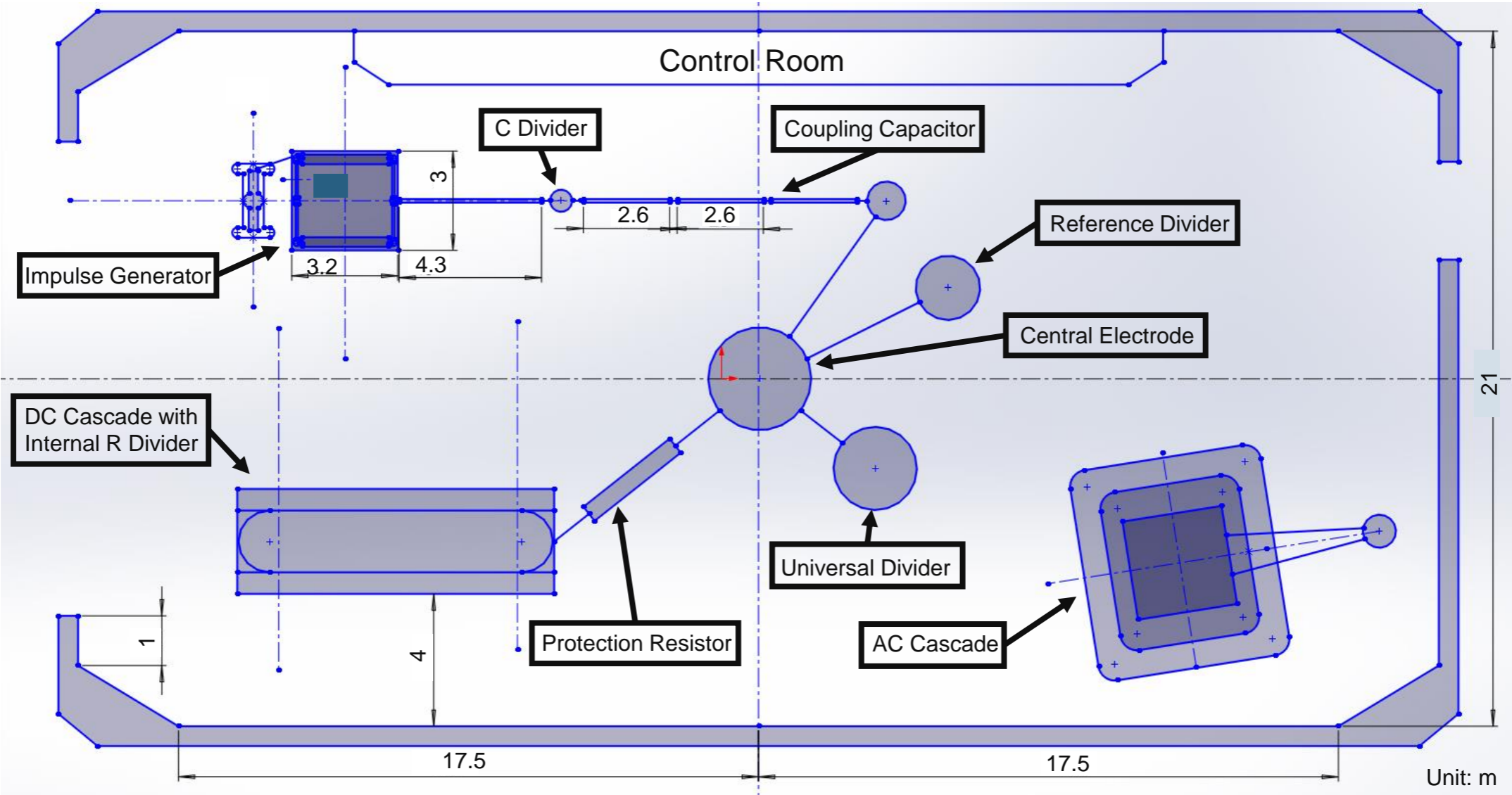


# Testing of protection resistor

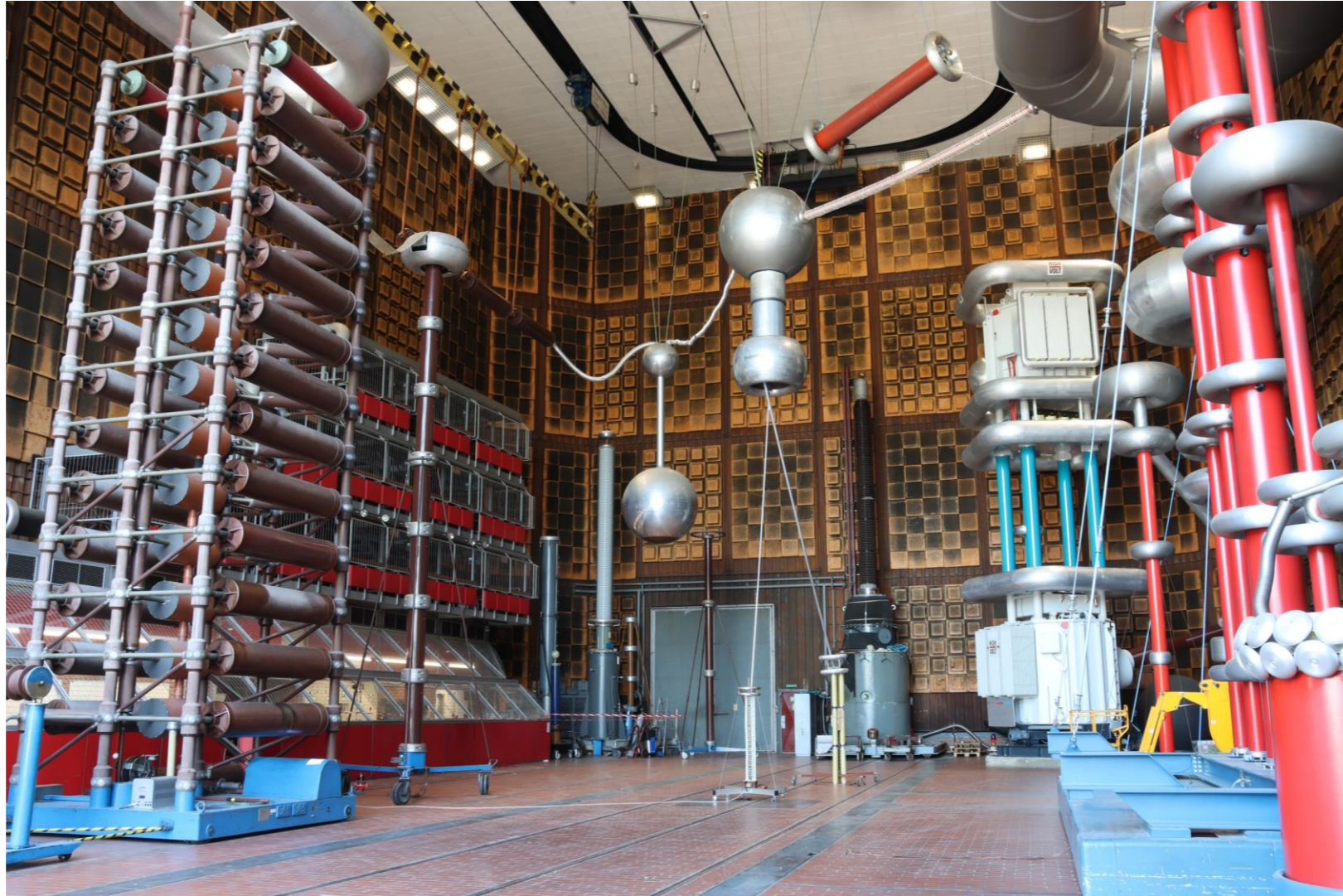
- LI at protection resistor
  - Negative polarity
  - Test voltage  $U = -250 \text{ kV}$  to  $U = -1300 \text{ kV}$  ( $\Delta U = -50 \text{ kV}$ )
  - Five impulses at each test voltage level
  - ✓ **LI passed**
  
- SI at protection resistor
  - Negative polarity
  - Test voltage  $U = -400 \text{ kV}$  to  $U = -1300 \text{ kV}$  ( $\Delta U = -50 \text{ kV}$ )
  - Five impulses at each test voltage level
  - ✓ **SI passed**



# Laboratory layout, birds view



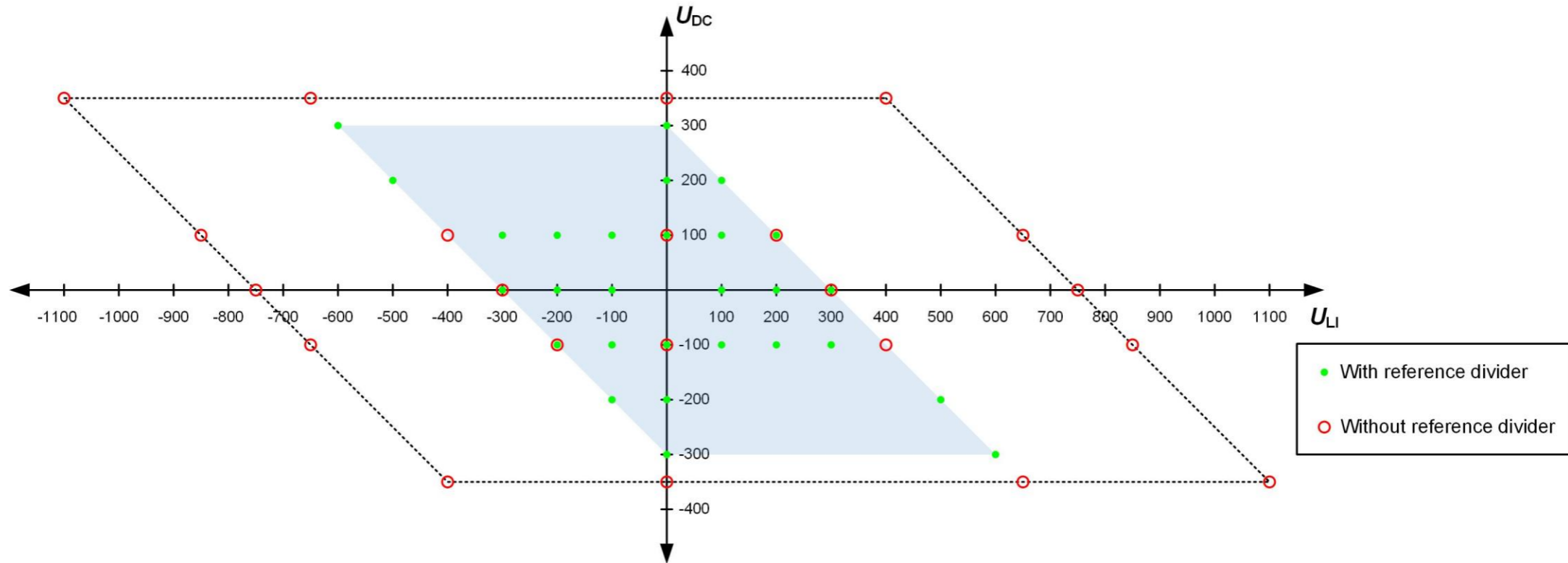
# Preliminary testing of test circuit



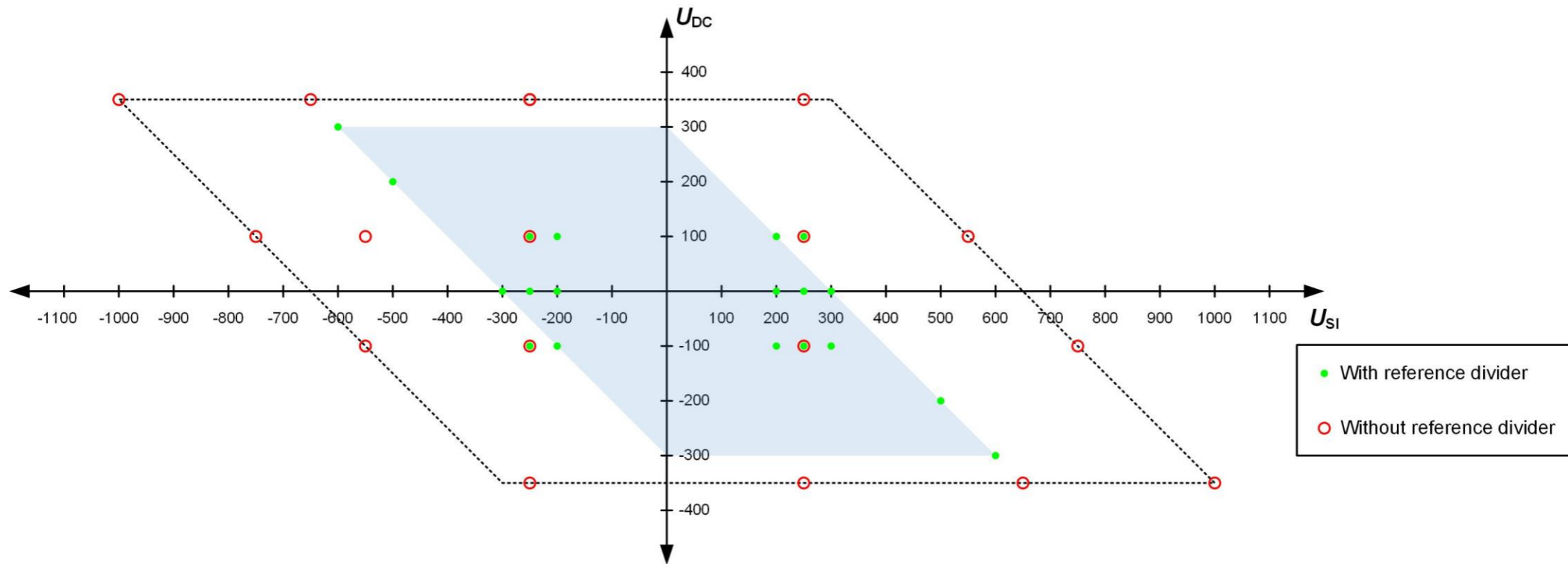
## Comparison campaign

- Three measurement systems based on universal voltage dividers (including recorder, software etc.)
  - Reference system (developed in HV-com<sup>2</sup>) ⇒ Ref
  - Two commercial systems from different manufacturers ⇒ Com1 and Com2
- Composite voltages only (blocking capacitor): DC+LI, DC+SI,  $n = 10$
- Reference divider limited to  $U \leq 300$  kV for HV to ground
- Commercial dividers limited to  $U \leq 750$  kV (DC+LI) and  $\leq 650$  kV (DC+SI) for HV to ground
- Two test sequences:
  - Sequence 1 ⇒ tests with reference divider:  $U_{DC} \leq 300$  kV,  $\hat{U}_{LI} \leq 300$  kV,  $\hat{U}_{SI} \leq 300$  kV
  - Sequence 2 ⇒ reference divider disconnected:  $U_{DC} \leq 350$  kV,  $\hat{U}_{LI} \leq 1100$  kV,  $\hat{U}_{SI} \leq 1000$  kV

# Test voltage range (DC/LI)



# Test voltage range (DC/SI)





# Comparison campaign

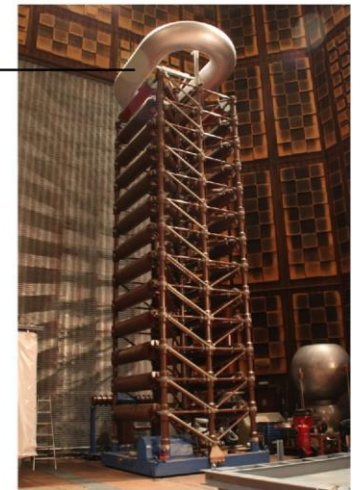
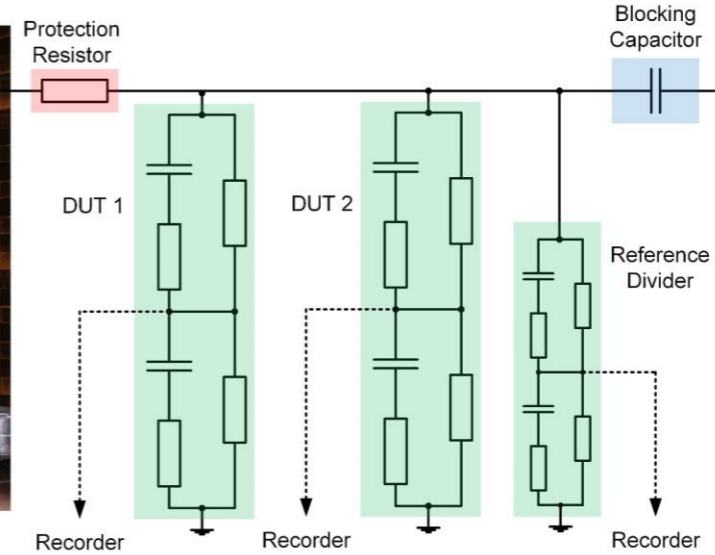
Sequence 1:

$$U \leq 300 \text{ kV}$$

$$U_{DC} \leq 300 \text{ kV}, \hat{U}_{LI} \leq 300 \text{ kV}, \hat{U}_{SI} \leq 300 \text{ kV}$$



DC: 1500 kV, 20 mA

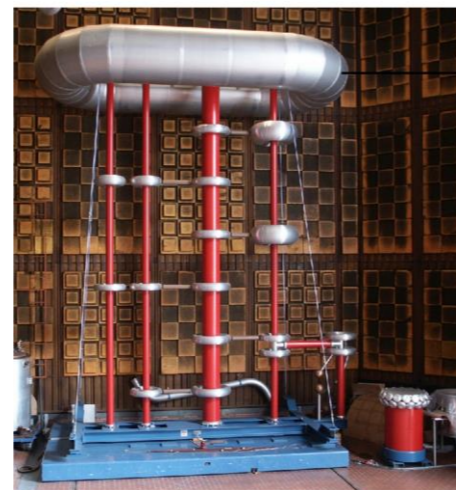


Impulse: 3250 kV, 165 kJ

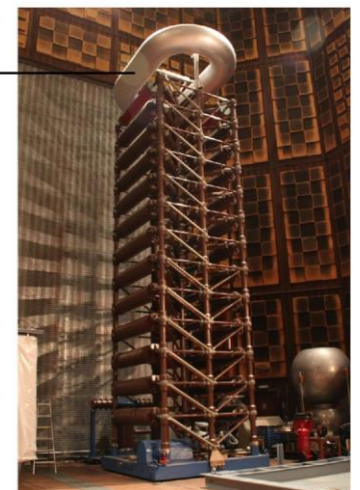
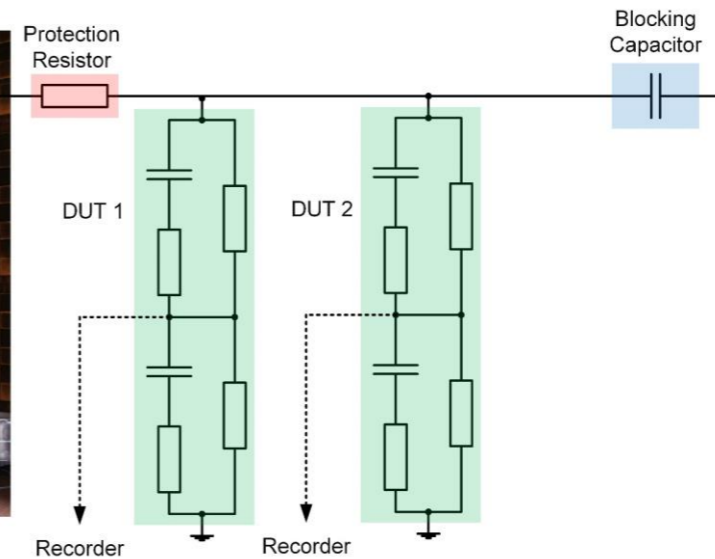
Sequence 2:

$$U \leq \pm 750 \text{ kV (DC+LI)}, U \leq \pm 650 \text{ kV (DC+SI)}$$

$$U_{DC} \leq 350 \text{ kV}, \hat{U}_{LI} \leq 1100 \text{ kV}, \hat{U}_{SI} \leq 1000 \text{ kV}$$



DC: 1500 kV, 20 mA

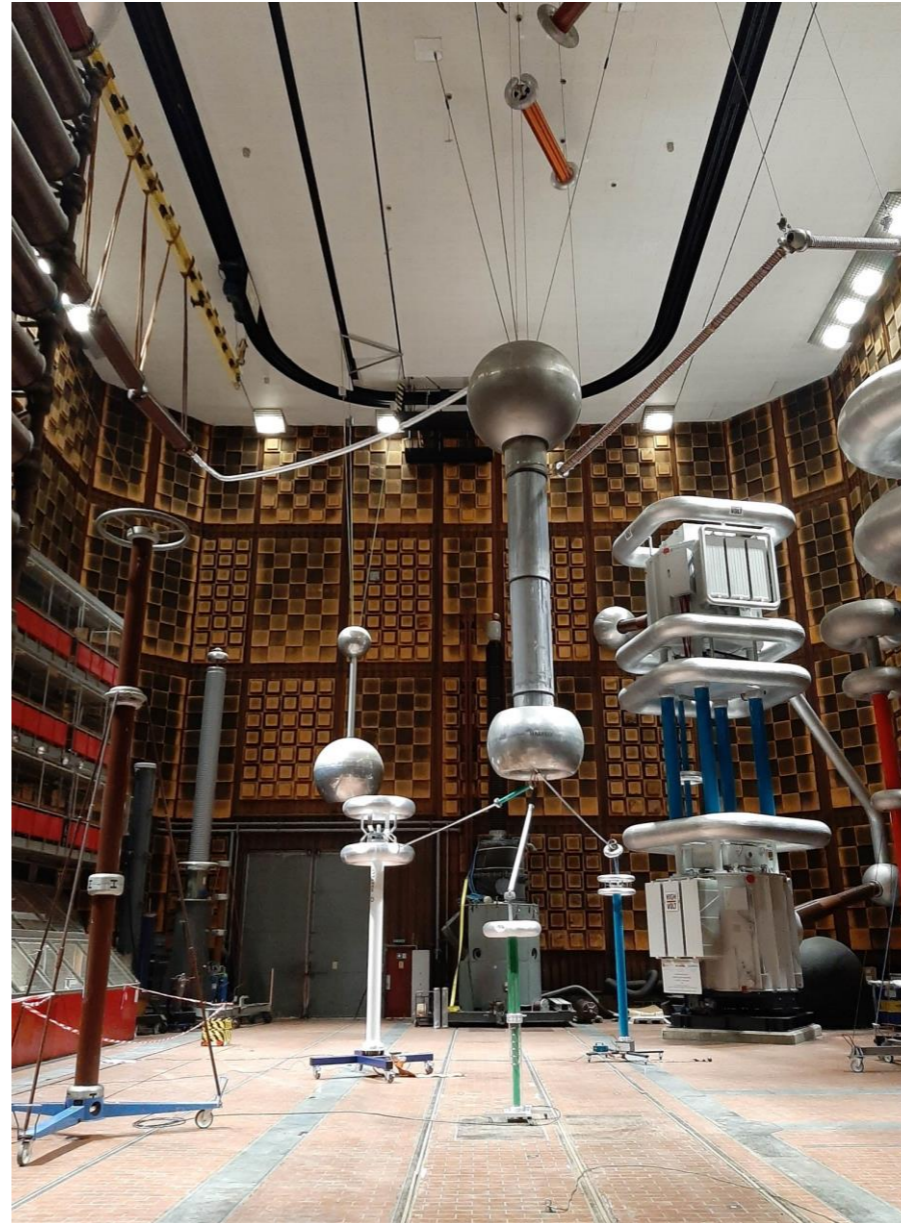


Impulse: 3250 kV, 165 kJ

# Comparison campaign

Complete test setup with  
 1 x reference divider  
 2 x commercial dividers

	Ref	Com1	Com2
$R$ in $G\Omega$	2,4	1	0,8
$C$ in pF	205	700	375
$R_D$ in $\Omega$	480	180	800
$R_{D-ext}$ in $\Omega$	529	355	207.5
max. $U_{DC}$ in kV	$\pm 300$	$\pm 600$	$\pm 400$
max. $U_{AC}$ in kV	300	400	400
max. $U_{LI}$ in kV	$\pm 300$	$\pm 1200$	$\pm 750$
max. $U_{SI}$ in kV	$\pm 300$	$\pm 1000$	$\pm 650$
Scale Factor $F$	820729	850	967
ADU	200 MHz 12 bit	250 MHz 16 bit	250 MHz 14 bit



# Evaluation

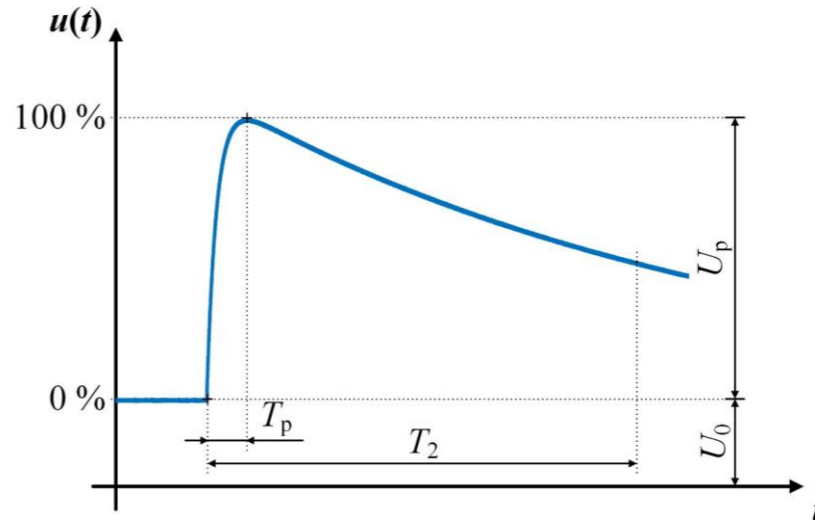
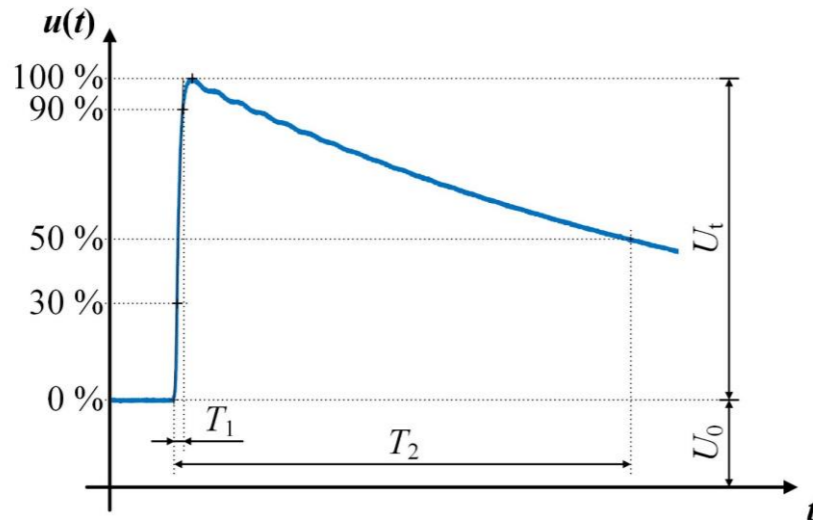
- Mean error ( $\Delta U_0$ ,  $\Delta U_t$ ,  $\Delta T_1$  etc):

- Sequence 1  $\Rightarrow$  com systems to ref system:

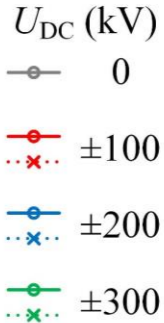
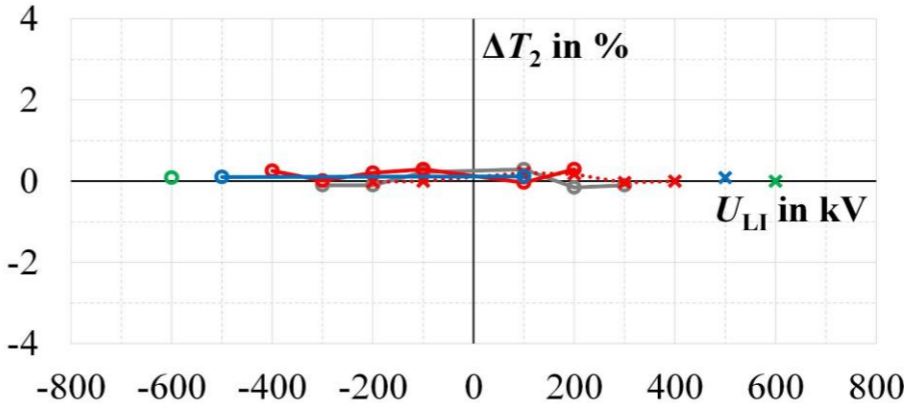
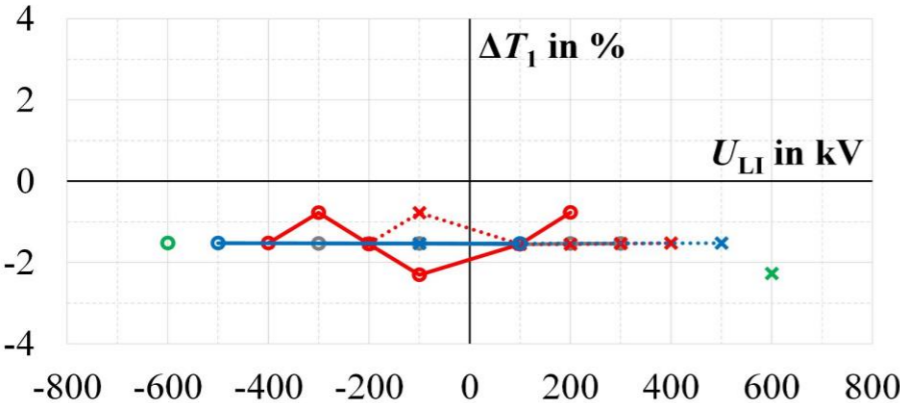
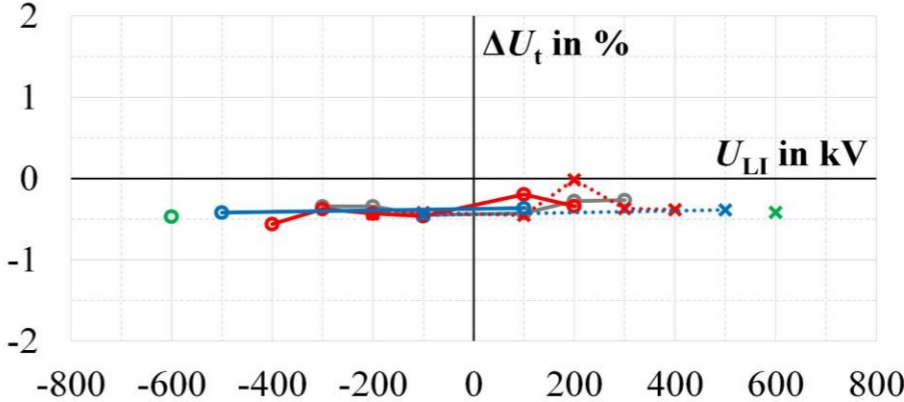
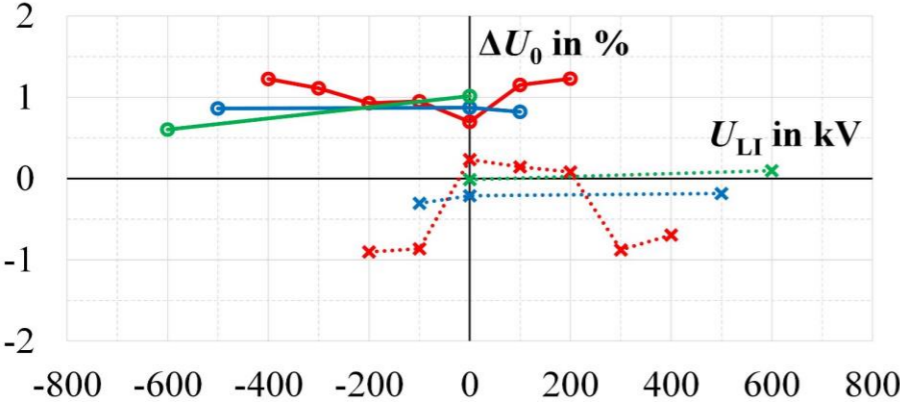
$$\text{e.g. } \Delta U_0 = \left( \frac{\frac{1}{10} \cdot \sum_{i=1}^{10} U_{0,\text{Com1/Com2},i}}{\frac{1}{10} \cdot \sum_{i=1}^{10} U_{0,\text{ref},i}} - 1 \right) \cdot 100\%$$

- Sequence 2  $\Rightarrow$  com1 to com2:

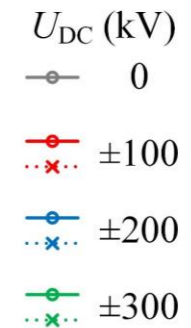
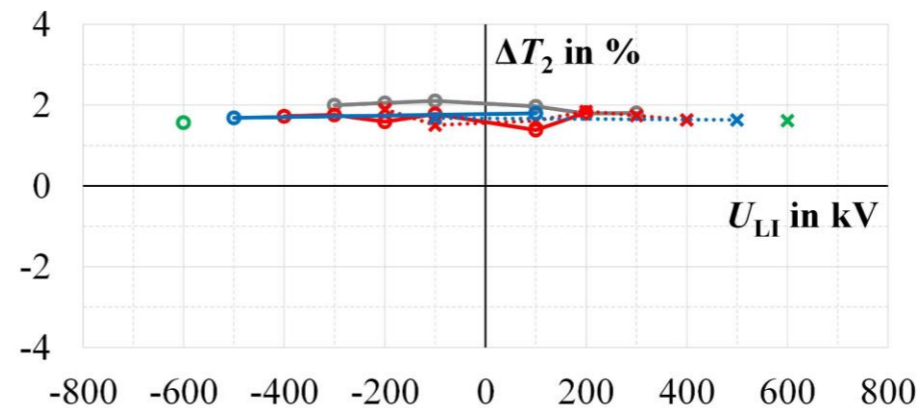
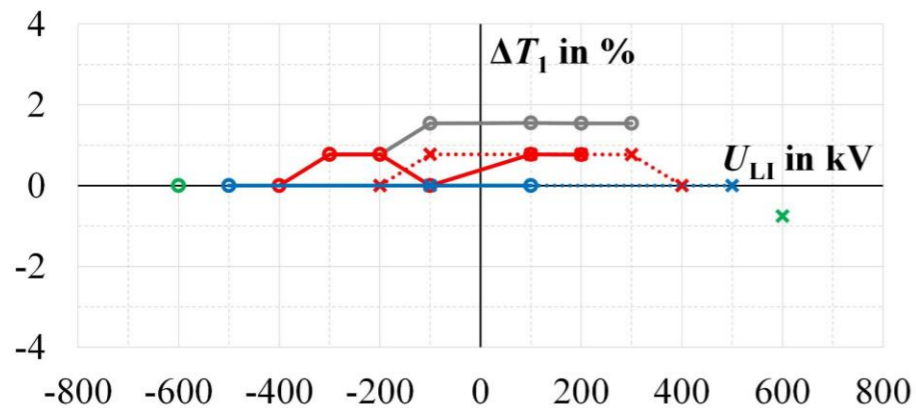
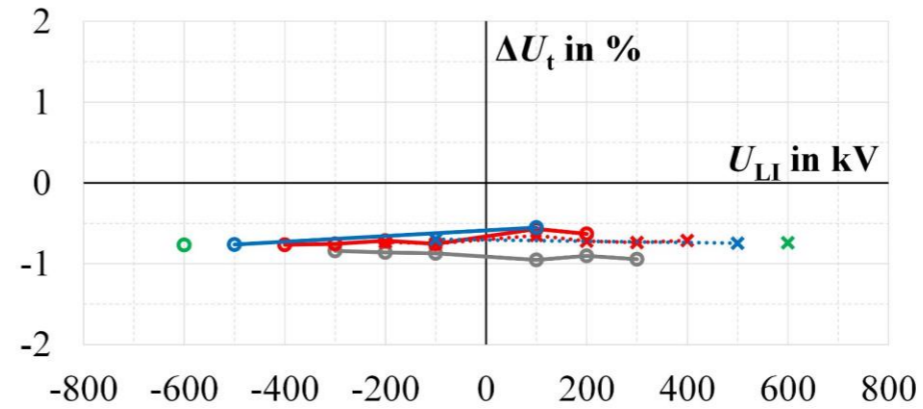
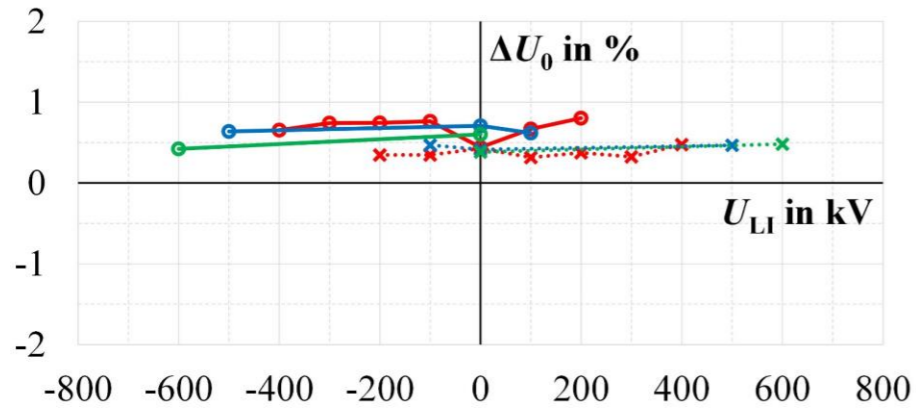
$$\text{e.g. } \Delta U_0 = \left( \frac{\frac{1}{10} \cdot \sum_{i=1}^{10} U_{0,\text{Com1},i}}{\frac{1}{10} \cdot \sum_{i=1}^{10} U_{0,\text{Com2},i}} - 1 \right) \cdot 100\%$$



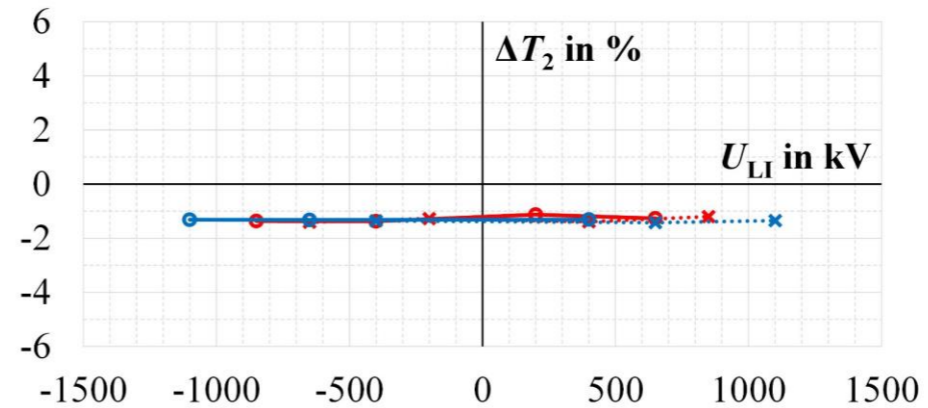
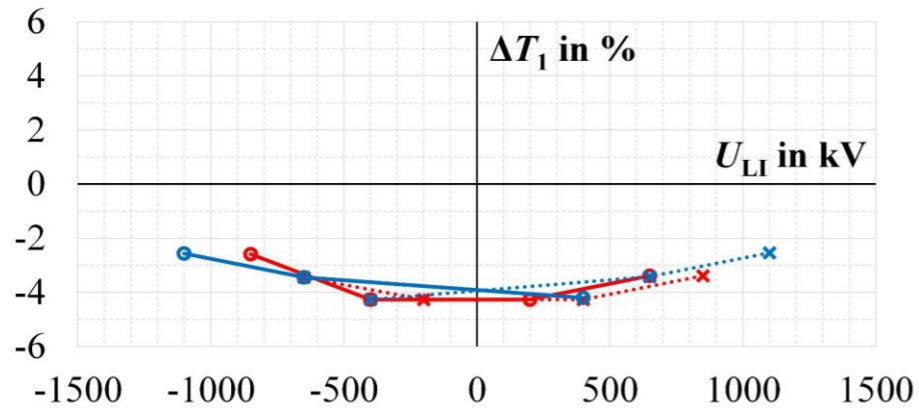
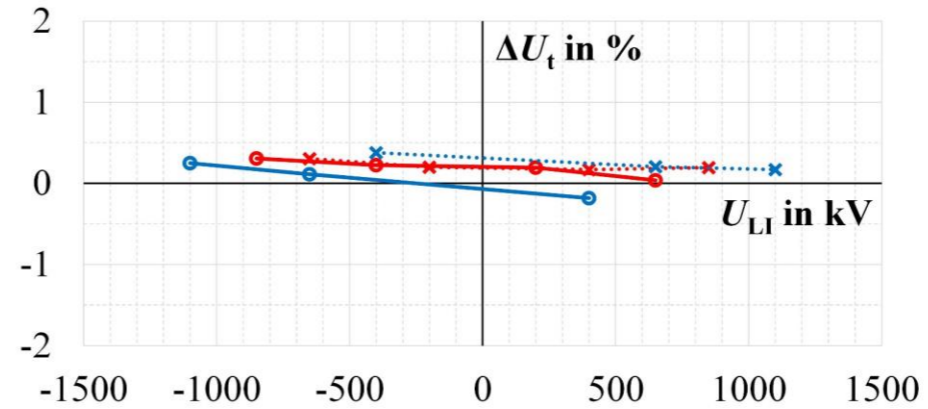
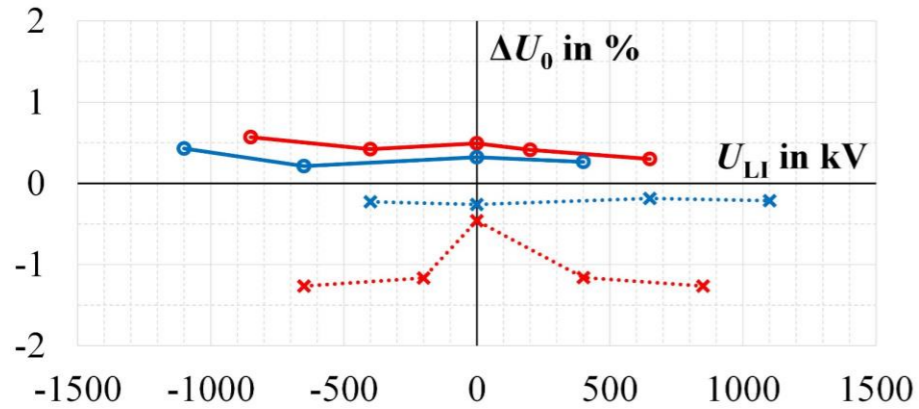
# Results DC+LI – Com1 to Ref



# Results DC+LI – Com2 to Ref

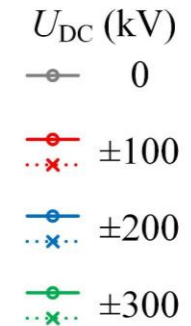
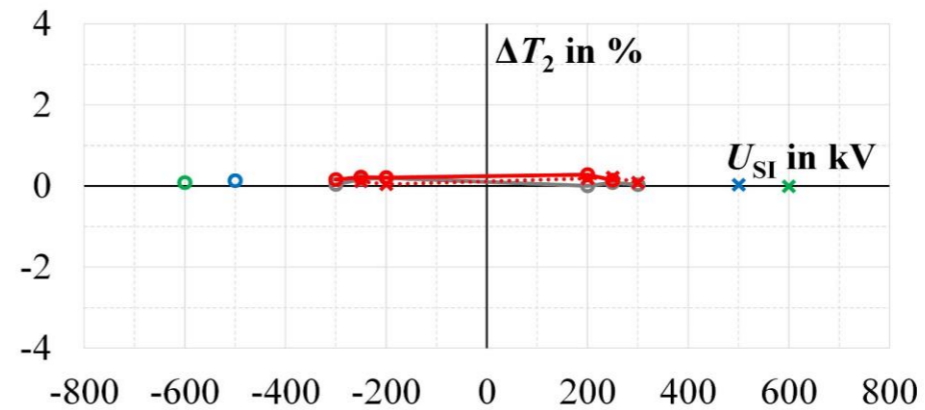
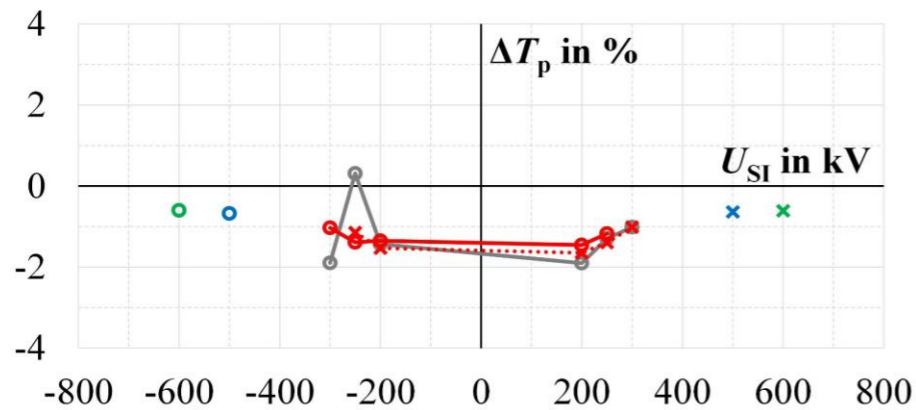
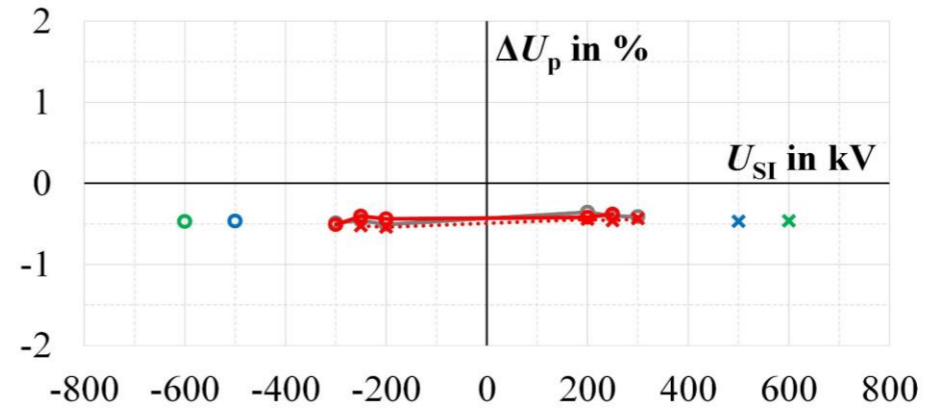
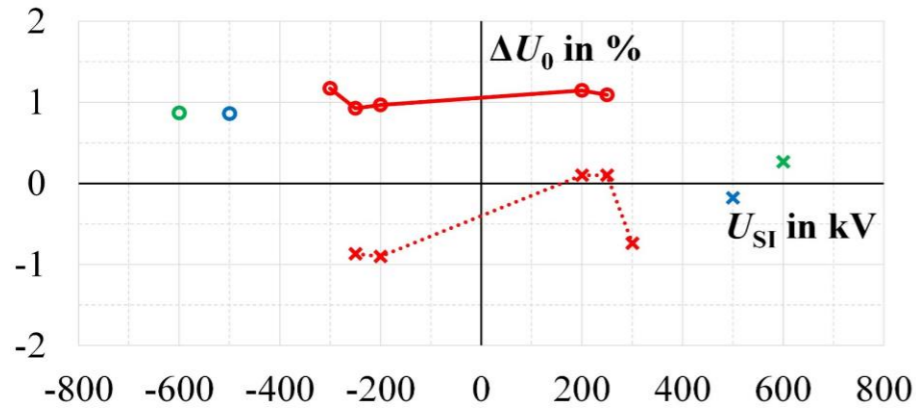


# Results DC+LI – Com1 to Com2

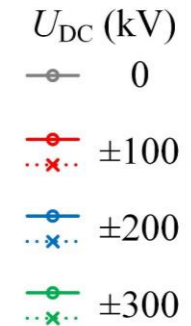
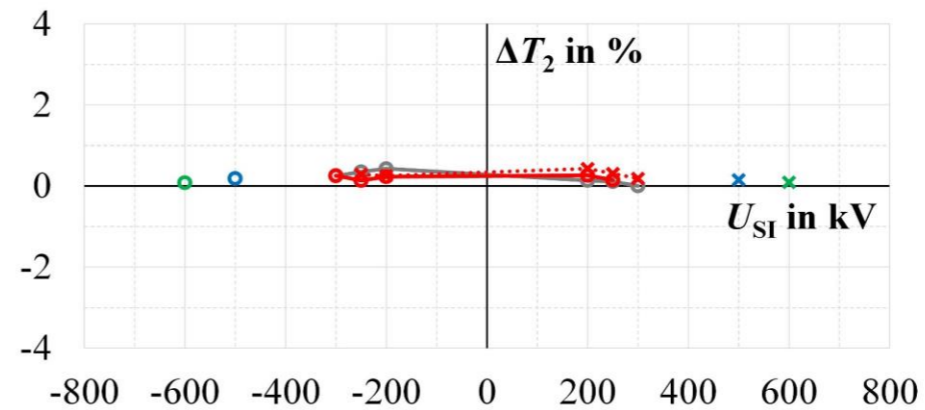
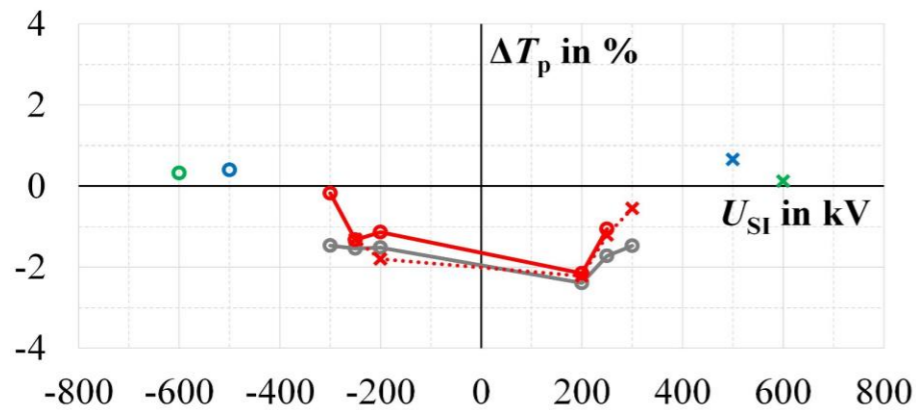
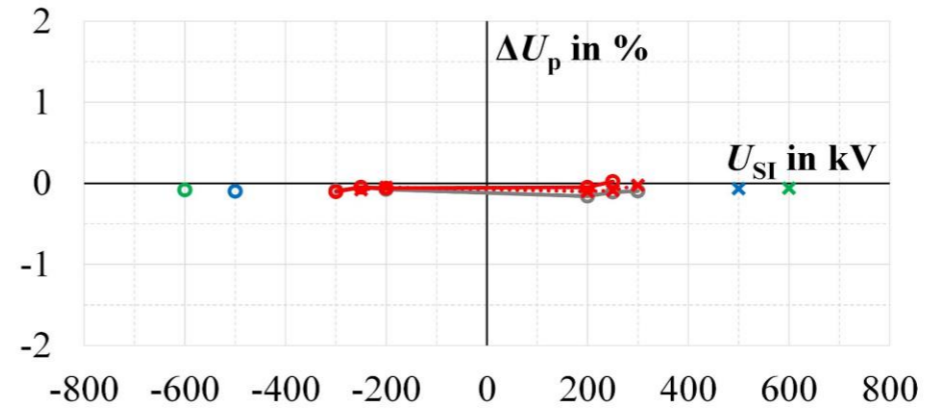
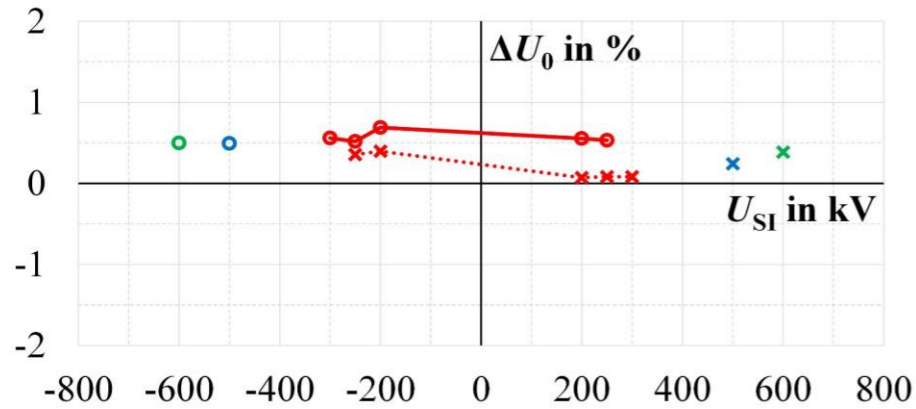


$U_{DC}$  (kV)  
 ●—●  $\pm 100$   
 ●—●  $\pm 350$

# Results DC+SI – Com1 to Ref

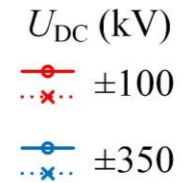
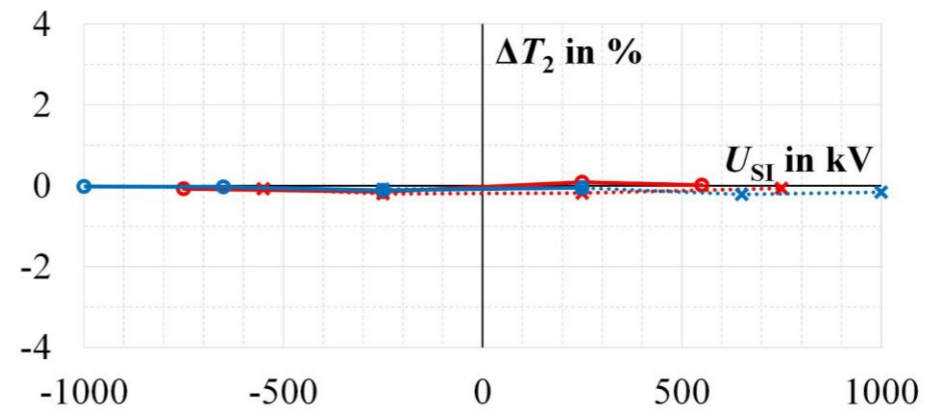
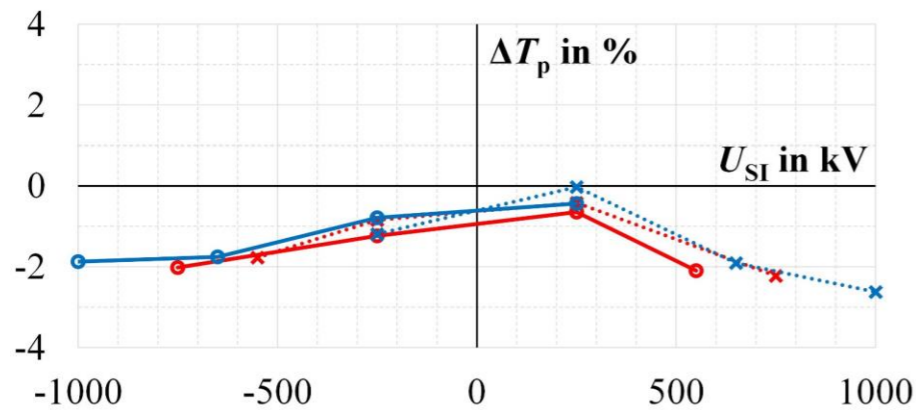
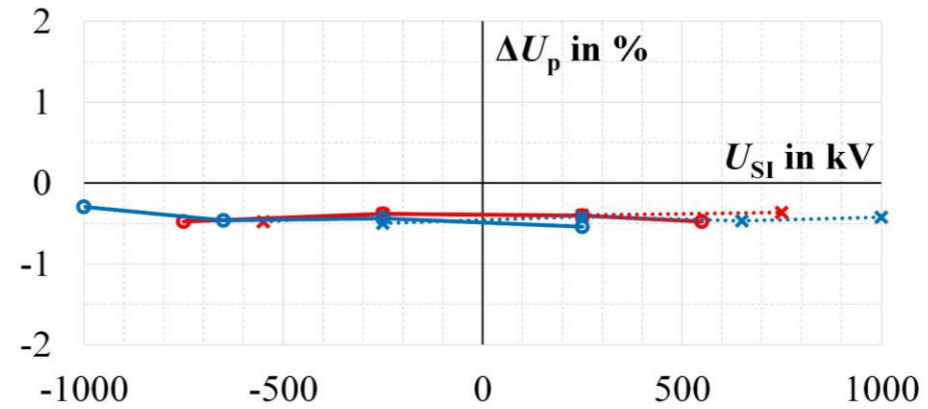
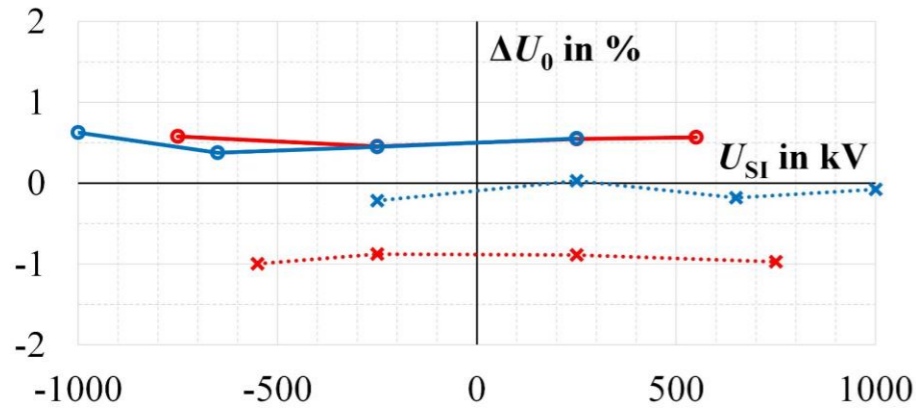


# Results DC+SI – Com2 to Ref





# Results DC+SI – Com1 to Com2



# Results – Summary

Min/max mean errors in % (DC+LI)

	$\Delta U_0$	$\Delta U_t$	$\Delta T_1$	$\Delta T_2$
<b>Com1/Ref</b>	-0.90	-0.56	-2.31	-0.15
	1.23	-0.01	-0,77	0.29
<b>Com2/Ref</b>	0.32	-0.95	0.76	1.38
	0.80	-0.55	1.55	2.10
<b>Com1/Com2</b>	-1.27	-0.18	-4.27	-1.42
	0.57	0.38	-2.54	-1.12

Min/max mean errors in % (DC+SI)

	$\Delta U_0$	$\Delta U_p$	$\Delta T_p$	$\Delta T_2$
<b>Com1/Ref</b>	-0.90	-0.54	-1.90	-0.01
	1.17	-0.36	0.31	0.28
<b>Com2/Ref</b>	0.07	-0.16	-2.39	0.00
	0.69	0.02	0.65	0.43
<b>Com1/Com2</b>	-1.00	-0.54	-2.63	-0.21
	0.63	-0.30	-0.03	0.09

## Conclusion

- Commercially available measurement systems based on universal voltage dividers are capable of analyzing DC+LI/SI superimposed voltages with the accuracy required for high voltage testing.
- All systems retained their high overall accuracy during all superimposed voltage tests, especially regarding their dynamic behaviour.
- A DC component did not have any negative effect on the performance of the measurement systems.
  
- It is sufficient to calibrate a measurement system based on universal voltage dividers for use with composite voltages with the respective individual voltages.
  - Scale factors for the different voltage waveforms should agree within  $\pm 1\%$ .
  - Deviation regarding time parameters should not exceed  $\pm 2\%$ .

# Publications

ISH 2021

## PREQUALIFICATION OF CAPACITORS FOR HIGH-PRECISION VOLTAGE DIVIDERS

*Hai Jiang<sup>1</sup>, Oliver Pischler<sup>\*1</sup>, Uwe Schichler<sup>1</sup>,  
Jussi Havunen<sup>2</sup>, Jari Hällström<sup>2</sup>,  
Ahmet Merev<sup>3</sup>, Serkan Dedeoglu<sup>3</sup>, Sami Özer<sup>3</sup>,  
Johann Meisner<sup>4</sup>, Stephan Passon<sup>4</sup>, Frank Gerdinand<sup>4</sup>*

ISH 2023

## PERFORMANCE OF UNIVERSAL VOLTAGE DIVIDERS FOR MEASUREMENT OF SUPERIMPOSED VOLTAGES

*Oliver Pischler<sup>1\*</sup>, Uwe Schichler<sup>1</sup>, Johann Meisner<sup>2</sup>, Stephan Passon<sup>2</sup>, Frank Gerdinand<sup>2</sup>,  
Jussi Havunen<sup>3</sup>, Jari Hällström<sup>3</sup>, Kari Lahti<sup>4</sup>, Frank Böhme<sup>5</sup>, Ralf Pietsch<sup>5</sup>,  
Mateusz Kujda<sup>6</sup>, Michael Gamlin<sup>6</sup>, Andreas Dowbysch<sup>7</sup>, Hans-Peter Pampel<sup>7</sup>*

CIGRE Symp. Cairns 2023



Paper title	Aspects of Standardization of RCR Dividers for Measurement of Composite Voltage on DC Cables and DC GIS/GIL
Study Committee	SC D1 - Materials and emerging test techniques

ISH 2023

## MEASURING HVDC-IMPULSE COMPOSITE VOLTAGES WITH HIGH-VOLTAGE DIVIDERS: LABORATORY COMPARISON AND ERROR ANALYSIS

*Andreas Dowbysch<sup>\*1</sup>, Hans-Peter Pampel<sup>1</sup>, Johann Meisner<sup>2</sup>, Frank Gerdinand<sup>2</sup>,  
Oliver Pischler<sup>3</sup>, Uwe Schichler<sup>3</sup>*

Measurement Campaign  
at TU Graz

...completed

